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## 93-0as

On the Kinematics of Incoherent Phase Transitions<br>Paolo Cermelli<br>Universita ${ }^{1}$ di Torino (Torino, Italy)<br>Morton E. Gurtin<br>Carnegie Mellon University<br>Research Report No. 93-NA-023

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b. Two-phase deformations

A two-phase deformation is described by a pair $\mathbf{y}_{\mathrm{n}}$ (Tt<oc,p) of deformations: $y_{n}$ associates with each material point $X$ in a closed region $B_{n}$ a point $x{ }^{*} y_{n}(X)$ of space. The points $X$ of $B_{n}$ are then the material points of phase $\mathrm{n}, \quad \mathrm{S}^{\wedge} \mathrm{y}^{\wedge} \mathrm{tB} \mathrm{B}^{\wedge}$ ) is the region of space occupied by phase it.

$$
\begin{equation*}
B=\mathcal{B}_{\mathrm{a}} \cup B \tag{2.2}
\end{equation*}
$$

is the deformed body, and

$$
\begin{equation*}
Z * \mathbf{S}^{\wedge} \mathbf{n S} \mathbf{S}^{\wedge} \tag{2.3}
\end{equation*}
$$

is the deformed interface (Figure 1). We write $\mathbf{Y}_{\mathrm{n}}$ for the inverse deformation:

$$
\begin{equation*}
\left.\left.X^{*} Y^{\wedge} x\right) \quad «^{*} \quad x<y^{\wedge} X\right) . \tag{2.4}
\end{equation*}
$$

We assume that $Z$ is a smooth (possibly unbounded) surface; the surface $S_{n}$ in $B^{\wedge}$ that deforms to $Z$,

$$
\begin{equation*}
\mathbf{S}_{\mathrm{n}} * \boldsymbol{Y}_{n}(Z), \tag{2.5}
\end{equation*}
$$

is the undeformed phase $n$ interface, it being tacit that the phases not separate at the interface. We emphasize that - to allow for incoherency we do not require coincidence of the undeformed interfaces $S_{a}$ and $S^{\wedge}$.

We assume henceforth that a two-phase deformation $\mathbf{y}_{\mathrm{n}}$ ( $\mathbf{n} * \boldsymbol{o c}, \mathrm{p}$ ) is prescribed. The invertibility (2.4) allows us to consider bulk fields as functions of position $\mathbf{x}$ in $B$, which is the spatial description, or as functions of the phase $T t$ and the material point $X$ in $B^{\wedge}$, which is the referential description. The spatial description is most convenient, as it allows a direct comparison of the fields at the interface; conversion to the referential description may be accomplished using the inverse mappings $\mathbf{Y}^{\wedge}$.

Precisely, a (spatially described) bulk field is a mapping ip that associates with each $\mathrm{xcB}, x t Z_{t}$ a scalar, vector, or tensor $\langle\mathrm{p}(\mathbf{x})$ with $\langle p(x)$ a smooth function of $x$ away from $Z$ and up to $Z$ from either side. For such a field, $\left\langle\mathrm{p}^{\wedge}\right.$ denotes the limit of $<\mathrm{p}$ from phase TT at the interface, while lq>] denotes the jump in $q>$ across the interface:

$$
\begin{equation*}
\varphi_{\pi}(x)=\lim _{z \rightarrow x} \varphi(z), \quad x \in \delta ; \quad[<p]=\varphi_{B}-\varphi_{\alpha} \tag{2.6}
\end{equation*}
$$

Analogously, inter/aciaJ fieids are functions of $\mathbf{x c} £$, examples being $q)^{\wedge}$ and [ $q>$ ]. (Fields subscripted by $n$ will generally denote interfacial fields associated with phase IT or bulk fields evaluated at the phase TI interface.)

We define the deformation gradient $F(x)$ at points $x$ away from the interface through

$$
\begin{equation*}
\left.\mathbf{F}(\mathbf{x}) * \mathbf{V} \mathbf{y}^{\wedge} \mathbf{X}\right) \tag{27}
\end{equation*}
$$

with $\mathrm{XcB}^{\wedge}$ the point that deforms to $x$, where the gradient $V$ in (27) is the material gradient (with respect to $X$ ).

We will consistently write, for $x \in \mathcal{S}$,
$\overline{\mathbf{n}}(\mathrm{x}) \quad$ for the unit normal to $Z$ directed outward from $x \in \partial B_{\alpha}$;
$n_{a}(x)$ for the unit normal to $S_{a}$ directed outward from $\mathrm{XcSB}_{\mathrm{a}}, \quad \mathrm{X}=\mathrm{Y}_{\mathrm{a}}(\mathrm{x})$;
$n_{p}(x) \quad$ for the unit normal to $S^{\wedge}$ directed inward from $X \in \partial B_{\beta}, X=Y_{B}(x)$.

Then

$$
\begin{equation*}
\bar{n}=\lambda_{\pi} F_{\pi}^{-\tau} n_{\pi}, \quad \lambda_{\pi}=\mid F_{\pi}^{-\top} n_{\pi} \Gamma^{-1} . \tag{2.8}
\end{equation*}
$$

Further,

$$
\begin{equation*}
P_{\pi}(\mathbf{x})=1-\mathbf{n}^{\wedge}(\mathbf{x}) ® n^{\wedge}(\mathbf{x}) \tag{2.9}
\end{equation*}
$$

is the projection of $R^{3}$ onto the tangent plane $\left.n^{\wedge} x\right)^{1}$ for $S_{\pi}$ at $X=Y_{\pi}(x)$,

We denote by

$$
\begin{equation*}
\mathbf{J} * \operatorname{det} \mathbf{F} \tag{2.10}
\end{equation*}
$$

the Jacobian of the deformation; the interfacial field

$$
\begin{equation*}
\delta_{\pi}=J_{\pi} / \lambda_{\pi} \tag{2.11}
\end{equation*}
$$

is then the surface Jacobian of the mapping that carries $S_{*}$ into $Z$.

## 3. INCOHERENCY TENSOR. BURGERS VECTORS

a. The incoherency tensor

Material points $X_{a} c S_{a}$ and $X^{\wedge} c S^{\wedge}$ will be referred to as compatible if they deform to the same point $x \in \mathcal{B}$ :

$$
\left.y \lll x_{a}\right)-y W .
$$

Such points are related by the mapping

$$
\begin{equation*}
\mathbf{h}(\mathbf{X}) \ll \mathbf{Y},\left(\mathbf{y}_{\mathbf{a}}(\mathbf{X})\right) \tag{3.2}
\end{equation*}
$$

from $S_{a}$ to $S^{\wedge}$ The tangential gradient $V_{a} h<V_{s_{\alpha}} h$ of $h$ maps tangent vectors $T$ to $S_{a}$ at $X$ into tangent vectors $\left(V_{a} h(X)\right) T$ to $S^{\wedge}$ at $h(X)$.

We will refer to

$$
\begin{equation*}
\mathbf{H}-\mathbf{F}^{\wedge} \mathbf{F}, \tag{3.3}
\end{equation*}
$$

as the incoherency tensor. $H$ and $V_{a} h$ coincide on tangents vectors: for all vectors $T$ tangent to $S_{a}$ at $X$,

$$
\begin{equation*}
\left(\mathbf{V}_{\mathrm{a}} \mathbf{h}(\mathbf{X})\right) \mathbf{T} * \mathbf{H}(\mathbf{x}) \mathbf{t}, \quad \mathbf{x}<\mathbf{y}_{\mathrm{a}}(\mathbf{X}) \tag{3.4}
\end{equation*}
$$

or equivalently, using (2.9),

$$
\begin{equation*}
\mathbf{V}_{\mathbf{a}} \mathbf{h}(X)=\mathbf{H}(\mathbf{x}) \mathbf{P}_{\mathbf{a}}(\mathbf{x}) \tag{3.5}
\end{equation*}
$$

The incoherency tensor also relates the orientations of the undeformed interfaces, since, by (2.8) and (3.3),

$$
\begin{equation*}
\mathbf{n}_{\mathrm{a}} \ll \mathbf{c o H}^{\mathrm{T}} \mathbf{n}^{\wedge}, \quad \mathbf{w} \ll\left(\mathbf{X}^{\wedge} / \mathbf{X}_{\mathbf{a}}\right) * \mathbf{I H}^{\mathrm{T}} \mathbf{n}^{\wedge} \mathbf{r}^{1} \tag{3.6}
\end{equation*}
$$

Choose compatible material points $X_{a}$ and $X^{\wedge}$, and let $x^{\wedge} y^{\wedge} X^{\wedge}$ ). Further, let $d X_{n}$ be an "infinitesimal line segment" on $S^{\wedge}$ at $X_{n}$, and let $d x_{t t}<F_{i r}(x) d X_{1 t}$. If $d x_{a}<d x^{\wedge}$, then $d X_{a}$ and $d X^{\wedge}$ are compatible (coincide
 infinitesimal line segments on the undeformed interfaces $S_{a}$ and $S_{r}$ If $d X p<d X_{a}$ for all compatible infinitesimal line segments, then the deformed lattices are - in some sense - coherent at $x$; and the same can be said if, for some symmetry transformation $Q, d X^{\wedge}{ }_{«} Q d X_{a}$ for all compatible infinitesimal line segments (Figure 2). This should motivate the following definition: the interface is infinitesimally coherent at $x c-\&$ if there is a $Q \in \mathscr{8}$ such that $H(X) T * Q T$ for all vectors $T$ tangent to $S_{a}$ at $X * Y_{a}(x)$,
or, more succintly,

$$
\begin{equation*}
\left.\mathbf{H}(\mathbf{x}) \mathbf{P}_{\measuredangle t}(\mathbf{x})-\mathbf{Q P J} \mathbf{x}\right) \tag{3.7}
\end{equation*}
$$

Thus infinitesimal coherence at a point $x$ on the deformed interface is the requirement that infinitesimal pieces of the two lattices "fit together" at $x$. The next proposition is a direct consequence of (3.7).

Proposition 3.1. Given a point $\mathbf{X} £ \&$ the following are equivalent:
(a) The interface is infinitesimally coherent at x .
(b) There is a Qc9 and a vector a such that

$$
\begin{equation*}
\mathbf{H}(\mathbf{x})=\mathbf{Q}+\mathbf{a}^{\circledR} \mathbf{n}_{\mathbf{a}}(\mathbf{x}) \tag{3.8}
\end{equation*}
$$

(c) There is a Qcg and a vector c such that

$$
\begin{equation*}
\mathbf{F}_{\mathbf{p}}(\mathbf{x}) \mathbf{Q}-\mathbf{F}_{\mathbf{a}}(\mathbf{x}) * \mathbf{c}{ }^{\circledR} \mathbf{n}_{\mathbf{a}}(\mathbf{x}) \tag{3.9}
\end{equation*}
$$

Fix the point $x$ and suppress it in what follows. Assume that the interface is infinitesimally coherent at $x$. Then the vectors $a$ and $c$ are given by

$$
\begin{equation*}
\mathbf{a} * \mathbf{H} \mathbf{n}_{\mathrm{a}}-\mathbf{Q} \mathbf{n}_{\mathrm{a}}, \quad \mathbf{c}=-\mathbf{F}_{\mathrm{p}} \mathbf{a} \tag{3.10}
\end{equation*}
$$

Further,

$$
\begin{equation*}
K-\mathbf{V} \quad \mathbf{n}, \cdot \mathbf{Q n}_{<} \tag{3.11}
\end{equation*}
$$

To establish (3.11), note first that, by (3.8),

$$
\begin{equation*}
\operatorname{det} H<\operatorname{det}\left(l+Q^{T} a^{\circledR} n_{a}\right) \ll 1+\left(Q^{T} a\right)-n_{a} \tag{3.12}
\end{equation*}
$$

On the other hand, (3.6) and (3.8) imply

$$
\begin{equation*}
\mathbf{c o - *} \mathbf{n}_{\mathrm{a}} * \mathbf{Q}^{\mathrm{T}} \mathbf{n}_{\mathrm{p}}+\left(\mathbf{a}<\mathbf{n}_{\mathrm{p}}\right) \mathbf{n}_{\mathrm{a}} \tag{3.13}
\end{equation*}
$$

so that $n_{a}< \pm Q^{T} n_{p}$; but by (3.12) the minus sign yields $\operatorname{co-}{ }^{1} n_{0 t}<-(\operatorname{detH}) n_{a}$, a contradiction, since $w$ and detH are strictly positive. Thus $n_{p} \ll n_{a}$. Further, this and (3.13) yield

$$
\begin{equation*}
\left(\mathbf{Q}^{T} \mathbf{a}\right)-\mathbf{n}_{\mathrm{a}} \ll\left(\mathbf{X}_{\mathrm{a}} / \mathbf{X}_{\mathrm{p}}\right)-\mathbf{1} ; \tag{3.14}
\end{equation*}
$$

since $\operatorname{det} H-J_{a} / J_{B}$, (2.11). (3.12), and (3.14) imply $J_{a}-J_{B}$.
b- Burgers vector. ${ }^{3}$ Burgers set
Given a curve $W$ in $R^{3}$, we write

$$
\begin{equation*}
\text { vector }(\mathbf{W}) *(\text { terminal point of } W)-(\text { initial point of } W) \tag{3.15}
\end{equation*}
$$

Let Iff be a closed curve in the deformed body with Iff a two-phase loop in the sense that iff intersects the interface exactly twice with corresponding undeformed curves

$$
\begin{equation*}
W_{n}<Y_{n}(\mathbf{1 f f}) \tag{3.16}
\end{equation*}
$$

nontrivial. Here $W^{\wedge}$ has orientation induced by Iff (Figure 3). The standard definition of the Burgers vector of $I f f$, in this setting, yields an expression

$$
\begin{equation*}
\int_{\mathbf{G}} \mathrm{F}^{-1}(\mathbf{x}) \mathrm{dx} * \operatorname{vector}\left(\mathbf{W}_{\mathrm{a}}\right) \cdot \operatorname{vector}\left(\mathbf{W}_{\mathrm{p}}\right) \tag{3.17}
\end{equation*}
$$

that is meaningless, since transformation of the references for phases oc and p by material isometries trarforms (3.17) to a vector of the form

$$
\begin{equation*}
\text { Qvector }\left(W_{\mathrm{a}}\right)+\overline{\mathbf{Q}} \operatorname{vector}(\mathbf{W},) \tag{3.18}
\end{equation*}
$$

with $Q, \bar{Q} c 9$ » and hence changes (3.17). ${ }^{4}$ Thus rather than a single Burgers vector for Iff there is a set $b(1 \mathrm{ff})$ consisting of all vectors of the form (3.18). We will refer to bttff) as the Burgers set for Iff. What is most important to us is the notion of a 'vanishing Burgers vector', which, within our framework, is the assertion that (3.18) vanish for some $\mathbf{Q}, \overline{\mathbf{Q}} \mathbf{9} 9$, or equivalently, that OcbClff). Letting $X$ and $Z$ denote the initial and terminal points of $W_{a}$, and $V^{\wedge}$ the portion of iff in phase $t$, we may use the group structure of $9^{\text {to }}$ express the condition OebClff) in the following equivalent forms (for some Qcfc):

[^0]\[

$$
\begin{align*}
& \text { Qvector }\left(\mathbf{W}_{\mathrm{a}}\right) \cdot \operatorname{vector}\left(\mathbf{W}_{\mathrm{p}}\right) \ll 0,  \tag{3.19}\\
& \mathbf{h}(\mathbf{Z})-\mathrm{h}(\mathrm{X}) \text { - QIZ-X], }  \tag{3.20}\\
& \underset{p}{ } \mathrm{JF}_{\mathrm{F}^{-}}{ }^{-1}(\mathrm{x}) \mathrm{dx} \cdot \mathrm{jQF}_{\mathrm{a}}{ }^{-1}(\mathrm{x}) \mathrm{dx} \ll 0 . \tag{3.21}
\end{align*}
$$
\]

Further, for $r^{*} \boldsymbol{a}, p$, if we let $\bar{W}^{\wedge}$ denote any curve on $S_{n}$ from the initial point of $W_{n}$ to its terminal point, then additional conditions equivalent to OcbHff) are (for son Qc9):

$$
\begin{align*}
& \text { Qvector }\left(\overline{\mathbf{W}}_{\mathrm{a}}\right)+\operatorname{vector}\left(\overline{\mathbf{W}}^{\wedge}\right) * 0_{\#}  \tag{3.22}\\
& \mathbf{J}(\mathbf{H}(\mathbf{x})-\mathbf{Q}) \mathbf{d X} \cdot 0 .  \tag{3.23}\\
& \bar{W}_{\alpha}
\end{align*}
$$

## 4. COHERENT SUBSURFACES

Let $C$ be a subsurface of $Z$, and write

$$
\begin{equation*}
C_{n}=Y .(C) \tag{4.1}
\end{equation*}
$$

for the subsurface of $S^{\wedge}$ that transforms to $C$. Then $C$ is infinitesimally coherent if the interface is anhnitesim ${ }^{\wedge} y$ coherent at each X€C. A much stronger restriction is the content of the next definition. We say that $C$ is coherent if there is a material isometry $f$ such that

$$
\begin{equation*}
X^{\wedge}<f\left(X_{a}\right) \text { whenever } X_{a} € C_{a} \text { and } X^{\wedge} e^{\wedge} \text { are compatible } \tag{4.2}
\end{equation*}
$$

(Figure 4). Thus infinitesimal coherence at $x$ is the requirement that infinitesimal segments of the lattices for the two phases fit together at $x$, while coherency for $C$ is the requirement that the lattices fit together over all of $C$. Note that (4.2) is equivalent to the assertion that $h$ restricted to $C_{a}$ is the restriction of a material isometry, so that, for some Qc9»

$$
\begin{equation*}
\mathbf{h}(\mathbf{Z})-\mathbf{h}(\mathbf{X})-\text { QIZ-X] } \quad \text { for all } \mathbf{X}, \mathbf{Z c C} \mathbf{C}_{\mathrm{a}} \tag{4.3}
\end{equation*}
$$

In comparing (3.20) and (4.3) it should be remembered that $Q$ in (3.20) depends on $X$ and $Z$, but $Q$ in (4.3) is constant. Note that, for $C$ coherent, not only is the set $C_{0}$ obtained by rigidly transporting the set $C_{a}$ by an isometry $f$, but, in addition, compatible points of $C_{a}$ and $C^{\wedge}$ are related through $I$. Note that, for $C$ coherent.

$$
\begin{equation*}
n_{p}(x)=Q n_{a}(x) \tag{4.4}
\end{equation*}
$$

for all xcC, where Qcfc corresponds to $f$.
By a two-phase loop for $C$ we mean a two-phase loop that passes twice through $\mathbf{C}$.

Theorem 4.1. Let $C$ be a subsurface of $Z$.
(i) C is coherent $«+\mathrm{C}$ is infinitesimally coherent;
(ii) C is connected and infinitesimally coherent -* C is coherent;
(iii) C is coherent ** Ocbttff) for any two-phase loop If for C ;
(iv) C is connected and Ocbttfi) for any two-phase loop Iff for $\mathrm{C} \bullet$

C is coherent.

We now prove this theorem.
(i) Let $C$ be coherent. Differentiating (4.3) with respect to $X$ on $C_{a}$ yields

$$
\begin{equation*}
\mathbf{V}_{\mathrm{a}} \mathbf{h}(\mathbf{X}) * \mathbf{Q P}_{\mathrm{a}}(\mathbf{x}) \tag{4.5}
\end{equation*}
$$

and, by (3.5), the required condition (3.7) for infinitesimal coherence is satisfied. (ii) Let $C$ be connected and infinitesimally coherent. Then, for each $X t C_{a}$,

$$
\begin{equation*}
\mathbf{V}_{\mathrm{a}} h(\mathbf{X}) \ll \mathbf{Q}(\mathbf{X}) \mathbf{P}_{\mathrm{a}}(\mathbf{X}) \tag{4.6}
\end{equation*}
$$

for some $Q(X) c 9$, where, for convenience, we consider $P_{a}$ as a function of $X$ rather than $x$. Choose arbitrary points $Z, \bar{Z} c C_{a}$. Since $C_{a}$ is connected we can find a smooth curve $W$ in $C_{a}$ from $Z$ to $\bar{Z}$. Let $X$ denote the set of all points $X c W$ with $Q(X) * Q(Z)$. Assume, for the purpose of contradiction, that $X * W$. Then, since $X$ is closed, there is a point Xc3X, XtfdW, such that $Q(\tilde{X}) * Q(Z)$. Further, since $\tilde{X} * d W$, there is a sequence $X_{n}->X, X_{n} c W$, such that, for each value of $n, Q\left(X_{n}\right) * Q(Z)$. By (4.6), $Q(X) P_{a}(X)$ is continuous along $W$. Thus $Q\left(X_{n}\right) P_{a}\left(X_{n}\right) * Q(X) P_{a}(\mathbb{X})$. But, since 9 is a finite group with orthogonal elements, and since $P_{a}(X)$ is continuous, this can happen only if $Q\left(X_{n}\right)<Q(X)<Q(Z)$ for all sufficiently large $n$, a contradiction. Therefore $X \ll W$ and $Q(Z)<Q(Z)$; hence $Q$ is constant on $C_{a}$. Finally, choosing $X, Z_{c C} C_{a}$ and integrating (d/da)h(Z)(cx)) along a smooth path $\mathbf{Z}(\mathbf{a}) \mathrm{c} \mathrm{C}_{a}$ with $\hat{\mathbf{Z}}(\mathbf{0}) * \mathbf{Z}$ and $\hat{\mathbf{Z}}(\mathbf{1}) * X$ yields

$$
\begin{equation*}
\left.\mathbf{h}(\mathbf{X})-\mathbf{h}(\mathbf{Z})<\underset{\mathbf{o}}{]} \underset{\mathbf{a}}{\mathbf{a}} \mathbf{h}(\hat{\mathbf{Z}}(\mathbf{a})) \hat{\mathbf{Z}}^{\prime}(\mathbf{a}) \mathbf{d a} * \mathbf{Q I X}-\mathbf{Z}\right], \tag{4.7}
\end{equation*}
$$

which, by (4.3), yields the coherency of $C$.
(iii) If $C$ is coherent, then there is a Qcfc such that (4.3) and (hence) (3.20) is satisfied.
(iv) Assume that C is connected and that OcbHff) for any twophase loop iff for $C$. Choose $X, Z_{c C}{ }_{a l}$ and let $x^{*} y_{a}(X)$ and $z^{*} y_{a}(Z)$ be the corresponding points on $C$. Since $Z$ is smooth, it is possible to construct a two-phase loop iff for $C$ that passes through $x$ and $y$; hence, by (3.20), there is a symmetry transformation $Q(X, Z)$ such that

$$
\begin{equation*}
\mathbf{h}(\mathbf{Z})-\mathbf{h}(\mathbf{X})<\mathbf{Q}(\mathbf{X}, \mathrm{ZHZ}-\mathbf{X}] . \tag{4.8}
\end{equation*}
$$

This relation must hold for all $\mathrm{X}, \mathrm{ZcC}_{\mathrm{a}}$; thus, since C is connected, an argument similar to that following (4.6) leads to the conclusion that $\mathbf{Q}(X, Z)$ is constant. Thus $\mathbf{C}$ is coherent.

## 5. TWO-PHASE MOTIONS

We now turn our attention to time-dependent situations. A twophase motion is a smooth one-parameter family $\mathbf{y}_{\mathbf{n}}(\mathbf{t})$ (ir<oc,p) of twophase deformations, the time $t$ being the parameter; thus, writing $y^{\wedge}\left(X_{f} t\right)<y_{11}(t)(X), y_{n}$ associates with each time $t$ and each material point $X$ in a closed region $B_{n}(t)$ a point $\left.x^{\wedge} y^{\wedge} t X / t\right)$. As before, $Y^{\wedge}$ is the (fixed-time) inverse of $y_{n}$,

$$
\begin{equation*}
\left.\mathbf{X}-\mathbf{Y}_{\mathbf{n}}(\mathbf{x}, \mathbf{t}) \quad{ }^{*} \quad \mathbf{x}-\mathbf{y}^{\wedge} \mathbf{X} . \mathbf{t}\right), \quad . * \tag{5.1}
\end{equation*}
$$

$\bigotimes^{\circledR} \mathrm{n}^{\wedge}<\mathrm{y}_{\mathrm{lc}}\left(\mathbf{B}_{\mathrm{lt}}(\mathrm{t}), \mathrm{t}\right)$ is the region of space occupied by phase $\mathbf{T I}$,

$$
\begin{equation*}
B(t) * S_{a}(t) u S^{\wedge}(t) \tag{5.2}
\end{equation*}
$$

is the deformed body,

$$
\begin{equation*}
\text { Zit }) * \mathbf{3}_{\mathrm{a}}(\mathrm{t}) \mathrm{nB},(\mathrm{t}) \tag{5.3}
\end{equation*}
$$

is the deformed interface, and

$$
\begin{equation*}
S_{\pi}(t)=Y_{\pi}(\delta(t), t) \tag{5.4}
\end{equation*}
$$

is the undeformed phase $n$ interface. We assume that $Z_{i}(t)$ evolves
smoothly with $t$.
We define the material velocity at points x away from the interface through

$$
\begin{equation*}
y-(x, t)<d y \wedge X / O / d t \tag{5.5}
\end{equation*}
$$

with $X € B_{n}(t)$ the point that deforms to $x$, where the derivative is the material time derivative (with respect to $t$ holding $X$ fixed). The remaining fields associated with the motion, such as the deformation gradient $F(x, t)$, are defined as before, but now depend on $t$.

## 6. INIERFACE VELOCITIES. SLIP

We write $\mathrm{V}^{\wedge}$ for the normal velocity of $\mathrm{S}_{\mathrm{n}}$ in the direction $\mathbf{n}^{\wedge}$ and $\overline{\mathbf{V}}$ for the normal velocity of $Z$ in the direction $\bar{n}$, with $V_{n}$ and $\overline{\mathbf{V}}$ both described spatially.

A vector function $z$ of time that satisfies $z(t) c £(t)$ for all $t$ is called a trajectory for $Z \backslash$ the normal component of $z^{\#}$ is then the normal velocity $\nabla$, so that

$$
\begin{equation*}
\mathbf{z -}(\mathbf{t}) * \mathbf{V}(\mathbf{z}(\mathbf{t}), \mathbf{t}) \overline{\mathbf{n}}(\mathbf{z}(\mathbf{t}), \mathbf{t}) \cdot(\mathbf{z}-)_{\tan }(\mathbf{t}), \quad(\mathbf{z}-)_{\tan }(\mathbf{t})-\overline{\mathbf{n}}(\mathbf{z}(\mathbf{t}), \mathbf{t})<\mathbf{0}, \tag{6.1}
\end{equation*}
$$

or more succintly,

$$
\mathbf{z}^{-} * \overline{\mathbf{V}} \overline{\mathbf{n}} \cdot\left(\mathbf{z o}_{\mathrm{tan}}, \quad\left(\mathbf{z}^{\#}\right) \tan -\overline{\mathbf{n}} *^{\circ} ;\right.
$$

if $\left(\mathrm{z}^{*}\right)_{\tan }<\mathbf{0}$, then z is a normal trajectory for \%. Normal trajectories satisfy the ordinary differential equation

$$
\begin{equation*}
z-(t) \quad 《 \quad \nabla(z(t), t) \bar{n}(z(t) f t) \tag{6.3}
\end{equation*}
$$

thus (granted sufficient regularity for $Z$ ), given an arbitrary time $t_{0}$ and an arbitrary point $\mathbf{x}_{0} \in<\&\left(t_{0}\right)$, there is exactly one trajectory $z$ through $\mathrm{x}_{0}$ at time $\mathrm{t}_{0}$, with $\mathrm{z}(\mathrm{t})$ defined for all t .

A similar definition applies to the trajectories $\mathrm{Z}^{\wedge}$ for $\boldsymbol{S}_{n}$. In this case,

$$
Z_{n}{ }^{*}(t)<V_{1 t}\left(Z_{n}(t), t\right) n_{1 T}\left(z_{t 1}(t), t\right) \wedge(Z /)_{U n}(t), \quad\left(Z_{t t^{-}}\right)_{\tan }(t)-n_{n}\left(z_{1 t}(t), t\right)<0
$$

where

$$
\begin{equation*}
\wedge(\mathbf{t})-\mathbf{y}_{\mathbf{n}}\left(\mathbf{Z}_{\mathbf{n}}(\mathbf{t}), \mathbf{t}\right) \tag{6.5}
\end{equation*}
$$

is the corresponding trajectory for $Z$. As before, we rewrite (6.4) in the abbreviated form

$$
\begin{equation*}
Z_{\pi}^{*}=V_{\pi} n_{\pi}+\left(Z_{\pi}\right)_{\tan }, \quad\left(Z_{\pi}\right)_{u^{*}} * \cdot \pi-0 . \tag{6.6}
\end{equation*}
$$

and refer to $\mathrm{Z}_{\mathrm{n}}$ as normal if $\left(\mathrm{Z}_{11}\right)_{\tan }<0$.
Given an arbitrary time $t_{0}$ and an arbitrary point $x_{0} € A\left(t_{0}\right)$, there is exactly one normal trajectory $Z_{n}$ through $\left.\mathrm{X}^{\wedge} \mathbf{V}^{\wedge} \mathrm{CX}^{\wedge} \mathrm{Q}^{\wedge}\right)$ at time $\mathrm{t}_{0}$. Letting $Z_{n}(t)$ denote the corresponding trajectory (6.5) for $Z$, we define

$$
\begin{equation*}
\left\langle\mathbf{y}_{w}\right)^{\#}\left(\mathbf{x}_{0} \cdot \mathbf{t o}\right\rangle-\mathbf{V}^{\wedge} \mathbf{o}^{*} . \tag{f>7}
\end{equation*}
$$

so that the interfacial field $\left(\mathrm{y}^{\wedge}\right)^{*}$ represents the time derivative of $\mathrm{y}^{\wedge}$ following the normal trajectories of the undeformed interface $S_{n}$. The trajectory $z^{\wedge}$ will generally not be normal, but $\overline{\mathbf{n}}^{*}\left(\mathbf{y}_{\text {Tr }}\right)^{\circ \subset} \overline{\mathbf{V}}$. By the chain rule,

$$
\begin{equation*}
\left(\mathbf{y}_{\mathbf{w}}\right)-«(\mathbf{y})_{\mathbf{n}} * \mathbf{V}^{\wedge} \mathbf{F}^{\wedge} \mathbf{n}^{\wedge} ; \tag{6.8}
\end{equation*}
$$

we therefore have the compatibility relation

$$
\begin{equation*}
\overline{\mathbf{n}}-\left(\mathbf{y} \%+V_{a} \bar{n}-F_{a} n_{a}<\bar{n}-(\mathbf{y})^{\wedge} \cdot V^{\wedge} \bar{n}-F^{\wedge},\right. \tag{6.9}
\end{equation*}
$$

or equivalently, appealing to (2.8),

$$
\begin{equation*}
\left\langle y V^{f i+x} a^{v}<^{e}\left(y^{\#}\right)^{\wedge}-n^{-*} x_{p} v_{p}<\bar{v}\right. \tag{6.10}
\end{equation*}
$$

We write

$$
\begin{equation*}
U_{\pi}=\bar{V}-\left(y^{*}\right)_{\pi} \cdot \bar{n}=\lambda_{\pi} V_{\pi} \tag{6.11}
\end{equation*}
$$

for the normal velocity of the deformed interface measured relative to the material of phase $t$.
(Possibly nonnormal) trajectories $\mathbf{Z}_{\mathbf{n}}$ for $\mathbf{S}^{\wedge}$ that satisfy

$$
\begin{equation*}
\left.\mathbf{y}^{*}\left(\mathbf{Z}_{\mathrm{a}}(\mathbf{t}) . \mathbf{t}\right)<\mathbf{y} / \mathbf{Z} \mathbf{p} \mathbf{W} . \mathbf{t}\right) \tag{6.12}
\end{equation*}
$$

for all $t$ are called compatible trajectories, as they correspond to the same trajectory for the deformed interface $Z$. Differentiating (6.12) we see that, for such trajectories,

$$
\begin{equation*}
\left(y^{*}\right)_{\alpha}+F_{\alpha} Z_{\alpha}{ }^{\cdot}=\left(y^{*}\right)_{\beta}+F_{\beta} Z_{\beta} \cdot \tag{6.13}
\end{equation*}
$$

Conversely, if (6.13) is satisfied for all time, and if (6.12) is satisfied at some time $t_{0}$, then the trajectories $Z_{n}$ are compatible.

The interfacial field

$$
\begin{equation*}
*-(\mathbf{y},)^{\circ}-\left(\mathbf{y}_{\mathrm{a}}\right)^{\circ} \tag{6.14}
\end{equation*}
$$

represents the interfacial slip; by (6.8),

$$
\begin{equation*}
\left.*-(y \% \cdot V\rangle_{p}-\langle\mathbf{y})_{a}-\mathbf{v}_{\mathrm{a}} \mathbf{F}_{\mathrm{a}} \mathbf{n}_{\mathrm{a}}-\mathrm{ly}\right)+\mathrm{rvmi} . \tag{6.15}
\end{equation*}
$$

Further, (6.6), (6.13), and (6.15) yield the alternative expression

$$
\begin{equation*}
»--W>\tan { }^{+} F \ll\left(Z_{a}\right)_{\tan } \cdot-I F\left(2^{\prime}\right)_{\tan } I \tag{6.16}
\end{equation*}
$$

for compatible trajectories $Z_{a}$ and $Z^{\wedge}$. If there is no slip, then, by (3.3),

$$
\begin{equation*}
(\mathbf{Z},)_{\tan }-\mathbf{H}\left(\mathbf{Z}_{\mathrm{a}} *\right)_{\tan } . \tag{6.17}
\end{equation*}
$$

and we have the following result.

Proposition 6.1. Assume there is no slip. Then, given any choice of compatible trajectories $\mathrm{Z}_{\mathrm{a}}$ and $\mathrm{Z}_{\mathrm{p}}$, if $\mathrm{Z}_{\mathrm{a}}$ is normal, then so also is $\mathrm{Z}_{\mathrm{p}}$.

## 7. PRODUCTION OF REFERENTIAL VOLUME

The field

$$
\begin{equation*}
\mathbf{W}^{\wedge}-\mathbf{V}^{\wedge}-\mathbf{I} V \mathbf{J} \tag{7.1}
\end{equation*}
$$

represents the flow of referential volume across the phase TT interface in the direction - $\overline{\mathbf{n}}$, per unit deformed area, and characterizes the production of lattice points at the interface.

Given a control volume (fixed region) $\mathbf{3 c}$ in the deformed body, if $\mathbf{m}$ denotes the unit outward normal to 3f, then
represents the rate at which referential volume is produced in !fc. A production of referential volume indicates a (positive or negative) production of lattice points (Figure 5) and, since atoms are conserved, this, in turn, signals a production of defects.

Proposition 7.1.
(a) $\mathrm{L}(\mathrm{tf}) * \mathrm{O}$ if 3 f lies solely in one phase.
(b) Let \& shrink to an arbitrary subset Q of $Z$. Then

$$
\begin{equation*}
L(\Re)--J[U / J] d a \ll-J l W l d a, \tag{7.3}
\end{equation*}
$$

$$
\mathbf{Q}
$$

so that

$$
\begin{equation*}
-\mathbf{I W}]<-[\mathbf{U} / \mathbf{J}] \tag{7.4}
\end{equation*}
$$

measures the interfacial volume-production rate, per unit deformed area.

To establish (a) assume that $\mathbf{B R}$ lies in one phase. Let $d_{t}$ denote partial differentiation with respect to $t$ holding $x$ fixed, and let grad and div denote the gradient and divergence with respect to $x$ holding $t$ fixed. Then differentiating the first term in (7.2) under the integral, applying the divergence theorem to the second, and combining the two integrals leads to an integral over $R$ with integrand

$$
\begin{equation*}
-J^{2} 3_{\mathrm{t}} \mathbf{J} \cdot \mathrm{~J}^{\wedge} \operatorname{divy}--\mathrm{J}^{2} \mathbf{y}^{*}-\operatorname{grad} \mathbf{J} \tag{7.5}
\end{equation*}
$$

but $\left.^{5} \mathrm{vT}^{*} \mathbf{J d i v y}{ }^{\prime} * \mathbf{c}\right)_{\mathbf{t}} \mathbf{J}+\mathbf{y}^{\#}<\operatorname{grad} \mathrm{J}$; hence (7.5) vanishes.
On the other hand, letting $\&$ contain and shrink to an arbitrary subset $Q$ of $i$, we find that
which, by (7.1) and (6.11), yields (7.3).

## 8. WHEN IS AN INTERFACE COHERENT?

We will refer to the interface $Z$ as coherent for all time if $£(t)$ is coherent at each $t_{f}$ and if the corresponding material isometry $f$ for $\%_{i}(t)$ is independent of $t$. Granted this, we may change reference configuration for phase a so that the material isometry $f$ is the identity. Therefore, without loss in generality, we may take $f$ to be the identity in the definition above, and this we shall do. Also, for consistency, the assertion " $8(0)$ is coherent" will have associated with it the requirement the material ${ }^{5}$ Cf.. t.g.. 1221. p. 62. «qt. (4); p. 72. «qt. (2).
isometry corresponding to $Z\{0)$ be the identity. A direct consequence of this definition is

Proposition 8.1. Let $Z$ be coherent for all time. Then:
(i) The undeformed interfaces coincide

$$
\begin{equation*}
\left.\left.\mathbf{S}_{\mathbf{a}}(\mathbf{t})<\mathbf{S}^{\wedge} \mathbf{t}\right) \ll S i t\right) . \tag{8.1}
\end{equation*}
$$

(ii) The motion is continuous across the interface in the sense that

$$
\begin{equation*}
\mathbf{y} «(\mathbf{X}, \mathbf{t}) * \mathbf{y},(\mathbf{X}, \mathbf{t}) \text { for all } \mathbf{X c S}(\mathbf{t}) . \tag{8.2}
\end{equation*}
$$

(iii) The normals and normal velocities coincide: for all $\mathrm{xc} £(\mathrm{t})$,

$$
\begin{equation*}
\mathbf{n}_{\mathrm{a}}(\mathrm{x}, \mathrm{t})<\mathbf{n},(\mathrm{x}, \mathrm{t}) \ll \mathrm{n}(\mathrm{x}, \mathrm{t}), \quad \mathbf{V}_{\mathrm{a}}(\mathrm{x}, \mathrm{t}) * \mathrm{~V}^{\wedge}(\mathrm{x}, \mathrm{t}) \ll \mathrm{V}(\mathrm{x}, \mathrm{t}) . \tag{8.3}
\end{equation*}
$$

A more important result is
Theorem 8.1. Suppose that the initial interface $Z(0)$ is coherent. Then the interface $Z$ is coherent for all time if and only if, at each time:
(a) the interface is infinitesimally coherent;
(b) the interfacial volume-production rate vanishes identically;
(c) the interfacial slip vanishes identically.

To establish this result assume first that the interface is coherent. Theorem 4.1(i) then implies (a). Next, differentiating (8.2) following an arbitrary normal trajectory of $S(t)$ yields, by (6.14), conclusion (c). Finally, (3.11)! and (8.3) imply that $W_{a}<W$, which is (b).

Conversely, consider an initially coherent interface consistent with (a)-(c) for all time. By (a), (3.11)! is satisfied. Thus (b), (7.1), and (7.4) imply that, for all $x \in \delta(t)$,

$$
\begin{equation*}
\mathbf{V},(\mathbf{x}, \mathrm{t}) * \mathbf{V}_{\mathrm{a}}(\mathbf{x}, \mathbf{t}) . \tag{8.4}
\end{equation*}
$$

Assume first that Zit) is connected. By (a) and Theorem 4.1(ii), Zit) is coherent at each $t$; thus the function $h$ defined by (3.2) at each $t$ is the restriction to $Z(t)$ of a material isometry

$$
\begin{equation*}
\mathbf{h}(\mathbf{X}, \mathbf{t})<\mathbf{Q X} * \mathbf{q}(\mathbf{t}), \tag{8.5}
\end{equation*}
$$

where $Q$ is independent of $t$, since 9 is discrete and $h(X, t)$ continuous
in $\mathbf{t}$; in fact, the initial coherence of the interface and our agreement in the first paragraph of the section yields

$$
\begin{equation*}
\mathbf{Q} * \text { 1. } \quad \mathbf{q}(\mathbf{0}) * \mathbf{0}, \tag{8.6}
\end{equation*}
$$

so that, by (4.4),

$$
\begin{equation*}
\mathbf{n}^{\wedge}(\mathbf{x}, \mathbf{t}) * \mathbf{n}_{\mathbf{a}}(\mathbf{x}, \mathbf{t}) *: \mathbf{n}(\mathbf{x}, \mathbf{t}) \tag{87}
\end{equation*}
$$

Next, let $Z_{a}$ and $2^{\wedge}$ be compatible trajectories; then, by definition, $Z_{a}(t)$ and $Z p(t)$ coincide in the deformed configuration and

$$
\begin{equation*}
\mathbf{Z}^{\wedge}(\mathbf{t}) \ll \mathbf{Z}_{\mathrm{a}}(\mathbf{t}) \cdot \mathbf{q}(\mathbf{t}) . \tag{8.8}
\end{equation*}
$$

Assume further, that $Z_{a}$ is normal (such trajectories always exist), so that, by (a), (c), and Proposition 6.1, $2^{\wedge}$ is also normal. We may therefore differentiate (8.8) and use (8.4) and (8.7) to conclude that $q^{\#}(t) \ll O$ for all $t$. But the initial coherence of the interface yields $q(0)<0$; hence $q(t) * 0$ for all $t$, and $h(X, t)$ is the identity on $S_{a}(t)$ at each $t$. Thus $Z$ is coherent.

If $Z$ is not connected, then the foregoing argument applied to each connected component of $Z$ again renders $h(X, t)$ the identity on $S_{a}(t)$, which completes the proof.

One can ask whether Theorem 8.1 remains valid if the no-slip condition (c) is omitted. To answer this let $\wedge(0)$ be coherent, and assume that the interface is infinitesimally coherent and that the interfacial volumeproduction rate vanishes identically. Then the results (8.4)-(8.8) remain valid, so that, by (8.4), (8.7), and (8.8),

$$
\begin{equation*}
\mathbf{q}-(\mathrm{t})-\mathbf{n}(\mathbf{x}, \mathrm{t}) * \mathbf{0} . \tag{8.9}
\end{equation*}
$$

Let us agree to call the interface cylindrical at $t$ if there is a unit vector $m(t)$, its axis, such that $x n(t)<n(x, t) * 0$ for all $x$. Then (8.9) is satisfied at a planar interface provided $q^{*}(t)$ is tangent to the interface, and at a cylindrical interface if $q^{*}(t)$ is parallel to the axis of the cylinder. In either case, we may use (6.16), (8.5), and (8.6) to conclude that the slip $V$ is given by

$$
\begin{equation*}
*--F^{\wedge} \mathbf{q}-<-F_{a} q \backslash \tag{8.10}
\end{equation*}
$$

On the other hand, if, at each $\mathfrak{t}$, Zit) is neither planar nor cylindrical, then $Z$ is coherent for all time.

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## APPENDIX ON LATTICES

a. Lattices. Invariant transformations

We use the term lattice to mean Bravais lattice. To describe these we write

$$
\begin{aligned}
\mathbf{V}^{3} * & \text { the set of all linearly independent } \\
& \text { triples }\left(\mathbf{g}_{1}, \mathbf{g}_{2}, \mathbf{B}_{3}\right) \text { with } \quad \mathbf{B j}^{\mathrm{dR} 3}>
\end{aligned}
$$

and given $\left(g_{1}, g_{2}\right.$ » $\left.\mathbf{g}\right) € \mathrm{~V}^{3}$, we say that $\mathrm{xclR}^{3}$ is an integer combination of the g 's if $\mathrm{x}-\mathrm{Mjgj}$ with $\mid \mathrm{i}_{\mathrm{lf}}\left\langle i_{2}\right.$, ${ }^{\text {anc }} *{ }^{*} \wedge 3$ integers (summation convention, from 1 to 3 , is implied for the subscripts $j$ and $k$ ).

A set $£$ of points of $\mathbf{R}^{3}$ is a lattice if $£$ is generated by a triple $(\mathrm{gi} * \mathrm{~g} 2 \cdot 83) €{ }^{*} \wedge^{3} *^{\mathrm{n}} \wedge$ e sense that $£$ is the set of all integer combinations of the g's. The gj are then called lattice vectors for $£$. Let
$7 \mathrm{ft} *$ the set of all $3 * 3$ matices $M$ whose determinant
is $\pm 1$ and whose entries $M j_{\mathrm{k}}$ are integers;
if

$$
\overline{\mathbf{g}} \mathbf{j}-\mathbf{M}_{\mathbf{j} \mathbf{k}} \mathbf{g}_{\mathbf{k}}, \quad \text { Mctni, }
$$

then ( $\bar{g}_{v} 62,63$ ) also generates $£$, and conversely (cf., e.g., Ericksen 118]).
Let $£$ be a lattice generated by ( $g_{1}, g_{2}$ "g3)- Given an invertible tensor $F$, we write

$$
F £ * \text { the lattice generated by }\left(\mathrm{Fg}^{\wedge} \mathrm{Fg}^{\wedge} \mathrm{Fgj}\right)
$$

a definition that is independent of the choice of lattice vectors $\quad\left(g_{1}, g_{2}{ }^{\text {® }} \mathbf{g}^{\wedge}{ }^{\wedge}\right.$ Note that

$$
\begin{equation*}
\mathfrak{£} \cdot<\mathbf{F} £ \quad++\quad T-i f \ll . \tag{Al}
\end{equation*}
$$

By an invariant transformation of $£$ we mean an invertible tensor G such that $\mathbf{G} £<\mathbb{£}$, or equivalently,

$$
\begin{equation*}
\mathbf{G g j} * \mathbf{M}_{\mathbf{j k}} \mathbf{g}_{\mathrm{k}} \text { for some } \operatorname{MctJl} \tag{A2}
\end{equation*}
$$

The point group $\mathbf{P}(\mathfrak{£})$ of $\mathfrak{£}$ is then the set of all orthogonal invariant transformations of $\mathfrak{f} \cdot$ Let $F$ and $G$ be invertible tensors. Then

G is an invariant transformation of $£$ «+
FGF ${ }^{\prime 1}$ is an invariant transformation of $F £$.
a result which follows from (AI) and the identity $\mathrm{FGF}^{\prime 1}(\mathrm{~F} £) * \mathrm{~F}$, which is valid if either $G$ is an invariant transformation of $£$ or $\mathrm{FGF}{ }^{11}$ is an invariant transformation of $\mathrm{F} £$.

Given any set $\mathbf{T}$ of tensors, we write $\mathrm{T}^{*}$ for the set of all tensors in $T$ with strictly positive determinant, so that
$\mathbf{P}(\mathfrak{£})^{+} *$ the set of all rotations (proper orthogonal
tensors) in the point group $\mathbf{P}(\mathfrak{£})$.

A direct consequence of (A3) is that, for any orthogonal tensor $Q$, $\mathbf{P}(\mathbf{Q})-\mathbf{Q P}(\mathfrak{f}) \mathbf{Q}^{\mathrm{T}}$ and $\mathbf{P}(\mathbf{Q} \mathfrak{f}) *{ }^{*} \mathbf{Q P}(\mathfrak{f})^{+} \mathbf{Q} \backslash$ so that if $F * R U$ is the polar decomposition of $F$ into an orthogonal tensor $Q$ and a positive definite, symmetric tensor $U$, then

$$
\begin{equation*}
\mathbf{P}(\mathbf{F} \mathfrak{f})+\text { « } \mathbf{Q P}(\mathbf{U} \mathfrak{£})+\mathbf{Q} \backslash \tag{A4}
\end{equation*}
$$

and similarly for the point group.
b. Relation of lattice theory to continuum theory. Admissibility sets for deformation gradients from a configuration with lattice $£$

Lattice theory is related to continuum theory through the CauchyBorn rule (cf. Ericksen 1191) in which a reference configuration of a body is a fixed region $B$ of $R^{5}$ together with a lattice $£(X)$ attached to each point XcB; $£(X)$ defines the microstructure of the body at $X$. Here we restrict attention to homogeneous bodies, for which there is a choice of reference configuration, called uniform, such that the reference lattice $£$ is independent of $X$. A deformation $y$ of $B$ then associates with each point $\mathbf{x} * \mathbf{y}(X)$ in the deformed region $S$ the lattice $F(X) £$.

We here limit our discussion to deformations for which - granted an appropriate choice of uniform reference configuration with lattice $£$ - the deformation gradient $F$ lies in an open srt 7 that excludes excessively large shears, but otherwise allows for finite deformations. In particular, we exclude from 7 those invariant transformations of $£$ that do not lie in the point group $\mathbf{P}(\mathfrak{f})+$. What seems to us to be a physically reasonable set of properties for 7 are (71)-(74) stated below; there and in what follows

$$
\operatorname{Lin}^{+} \text {« the set of all tensors } F \text { with } \operatorname{det} F>0
$$

and we write " F is admissible" to signify that Fc 7.
(71) 7 is an open subset of Lin*.
(72) 1 is admissible,
(73) $\mathbf{Q F}$ is admissible for all admissible $\mathbf{F}$ and all rotations $\mathbf{Q}$.
(74) Let F be admissible. Then $\operatorname{GcP}(£) *$ if and only if FG is admissible and $\mathrm{FGF}^{\mathbf{1 1}}$ is an invariant transformation of F .

A set 7 with properties (71)-(74) will be referred to as an admissibility set for deformations from a reference configuration with lattice $£$.

In the reference configuration the deformation gradient $F$ is the identity; hence the restriction (72). (73) is the requirement that if the deformed body is rigidly rotated, the resulting deformation gradient remains in 7. (74) requires more explanation. The reference configuration has $£$ as its lattice. Taking $\mathrm{F}=\mathrm{l}$ in (74) yields the conclusion:
(75) An admissible $G$ is an invariant transformation of $£$ if and only if $\mathbf{G} \in \mathbb{P}(\mathcal{L})^{+}$.

Thus the only admissible invariant transformations of the reference lattice are rotations in its point group so that, in some sense, the reference configuration is undistorted with cspect to 7. But (74) asserts more. If we deform the body $B$ with (constant) deformation gradient $F$, then $F £$ is the lattice in the deformed body $S$, and (74), a consistency condition, asserts that the invariant transformations of F £ with FG admissible are exactly those induced in the natural manner from rotations in the point group $\mathbf{P}(£)$.

Another consequence of (72)-(74) is:
(76) Let $F$ be admissible and let $G$ be an invariant transformation of £. Then $\mathbf{G}$ is admissible if and only if FG is admissible.

In fact, granted (73),

$$
\begin{equation*}
(74)<*(75),(76) . \tag{A5}
\end{equation*}
$$

The implication (74) -+(75) has already been established. The remainder of (A5) follows upon using (A3). (72M74) also imply
(77) If $U$ is admissible, symmetric, and positive definite, then $\mathbf{P}(\mathbf{U} \text { £ })^{+} \mathbf{C P}(\mathfrak{£})^{+}$; in fact,

$$
\begin{equation*}
\left.\mathbf{P}(\mathbf{U} \mathfrak{E})^{+} * \text { the set of all } \mathbf{Q c P t e}\right)^{*} \text { such that } \mathrm{QUQ}^{\mathrm{T}}<\mathbf{U} . \tag{A6}
\end{equation*}
$$

This result with (A4) yields the conclusion that if $F \ll R U$ is the polar decomposition of an admissible $\mathbf{F}$, then $\mathbf{P}(\mathbf{F} \mathfrak{f}) * \operatorname{CRP}(\mathfrak{f}){ }^{+} \mathbf{R}^{\mathrm{T}}$.

For any lattice $£$ ', let
*y $\left(£^{\S}\right)$ * the group of invariant transformations of $£ \backslash$
To verify (77), choose $\operatorname{RcP}(\mathbf{U}) *$. Then $\operatorname{Rc}^{\#} \mathbf{y}(\mathrm{U} £)$, so that, by (A3), U-iRUcVO. Hence RU《UF with $F^{\wedge} \wedge(£)$. By (73), RUc7; hence UFc7 and (76) yields Fc7. Thus $\mathrm{Fc}_{\mathrm{H}} \mathrm{n}^{\mathrm{f}} \mathrm{y}(\mathrm{f})$, so that, by (75), $F^{*} \mathbf{Q c P}(£)^{+}$- Therefore $\mathbf{R U}=\mathbf{Q}\left(\mathbf{Q}^{T} \mathbf{U Q}\right)$, and by the uniqueness of the polar decomposition of a tensor, $R « Q$ and $U * Q^{T} U Q$. These conclusions yield the validity of (77).

The following result, which we shall prove in Subsection d, is a direct corollary of a theorem of Ericksen and Pitteri.

Existence theorem for admissibility sets. Given any lattice $£$ there exists an admissibility set 7 for deformations from a reference configuration with lattice $£$.

## c. Two-phase systems

Our discussion in the body of the paper is based on a single reference lattice $£$ in conjunction with symmetry transformations of $£$ that are rotations. We now use the theory developed in this Appendix to justify these suppositions.

Consider a two-phase system with phases a and $p$. Choose fixed uniform reference configurations for a and $p$ with corresponding lattices $\mathfrak{f}_{\mathrm{a}}$ and $\mathfrak{f}^{\wedge}$. Let $7_{a}$ and $7^{\wedge}$ denote admissibility sets for a and $p$ for deformations from their respective reference configurations. At this point it
is most convenient to view the admissibility sets $T_{a}$ and $¥_{p}$ as unrelated; that is, as lying in unrelated copies of Lin .

The phases may be related by choosing a tensor $U$ such that

$$
\begin{equation*}
\mathfrak{£}, \ll \mathbf{U}_{\mathrm{a}} . \tag{A7}
\end{equation*}
$$

What is important, we assume that there is a choice of $U$ such that $\mathrm{U} € 7_{\mathrm{a}}$; granted this we may, modulo a rigid rotation of the reference configuration for oc, choose $U$ to be symmetric and positive definite. By (77), a consequence of this assumption is that the point groups for $\mathfrak{£}_{\mathrm{a}}$ and £p satisfy

$$
\begin{equation*}
\mathbf{P}\left(£^{\wedge}\right) \mathbf{c} \mathbf{P}\left(£_{a}\right) \tag{A8}
\end{equation*}
$$

thus a represents a parent phase, p a product phase.
Consider the set $S_{a p}$ of all a-admissible transformations of $£_{\mathrm{a}}$ into $£_{\&}$ :

$$
\begin{equation*}
\mathbf{J}_{\mathrm{a}}{ }^{\wedge} * \text { the set of all } \mathrm{V} \mathbf{c} ?_{\mathrm{a}} \text { such that } \mathfrak{£}^{\wedge} * \mathbf{V} \mathfrak{£}_{\mathrm{a}} . \tag{A9}
\end{equation*}
$$

Choose Vc3 ${ }_{a b}$. Then, by (A9), $V £_{a} * U £_{a}$, so that $6^{*} V^{\prime \prime 1} U$ is an invariant transformation of $\mathfrak{f}_{\mathrm{a}}$. Trivially, $\mathrm{U}<\mathrm{VG}$ with both $U$ and $V$ in $7_{a}$; we may therefore conclude from (76) that $G € 7_{a}$, so that, by (75), G and hence $G^{r 1}$ belongs to $P\left(£_{a}\right)^{+}$. Thus every $V c \$_{a}{ }^{\wedge}$ may be written in the form $V^{*} \mathrm{UQ}, \operatorname{QcP}\left(£_{\mathrm{a}}\right)^{+}$. Since, trivially, the converse is also true, $S_{a p}$ is the set of all tensors UQ, $\operatorname{QcP}\left(£_{\mathrm{a}}\right)^{+}$:

$$
\begin{equation*}
{ }^{*}<^{*}{ }^{s} \mathbf{U} P(\mathbf{C} / . \tag{A10}
\end{equation*}
$$

Note that, using the right coset decomposition of $\mathbf{P}\left(£_{a}\right) *$ with respect to $P(£ p)^{*}$, we can also write $J_{a p}$ as the set of all tensors of the form $Q^{\wedge} \mathbf{U Q}_{a}$ with $\left.\mathbf{Q}_{\mathrm{a}} € \mathbf{P}\left(\boldsymbol{£}_{\mathrm{a}}\right)^{+}{ }_{f} \mathbf{Q}^{\wedge} € \mathbf{P}(£)\right)^{*}$; that is, $\mathrm{J}_{\mathrm{a}}, \ll \mathbf{P}\left(\mathbf{t} / \mathbf{U P}\left(\boldsymbol{£}_{\mathrm{a}}\right)^{+}\right.$.

The theory developed in the body of the paper is easily formulated within the current framework involving "unrelated" references for the two phases. In particular, the discussion of two-phase deformations would now carry the restrictions $\mathrm{F}_{\mathrm{a}} € 7_{\mathrm{a}}$ and $T_{p} € 7_{p}$ on the deformation gradients but would otherwise remain essentially unchanged. (Here we use the * to differentiate the current theory from that discussed in the body of the paper.) The definition of infinitesimal coherency at $x$ would now be the


$$
\begin{equation*}
\mathbf{f i}(\mathbf{x}) \mathbf{P}_{\mathrm{a}}(\mathbf{x})=\mathbf{G} \mathbf{P}_{\mathrm{a}}(\mathbf{x}) \quad \text { for some } \quad \mathbf{G c} \mathbf{J}_{\mathrm{ap}} \tag{All}
\end{equation*}
$$

and similar changes apply to the material on Burgers vectors.
To convert this theory to the theory discussed in the body of the paper, we change reference configurations for $p$ so that its reference lattice coincides with that of $a$. We accomplish this by a change in reference configuration via the tensor $U$; precisely, we change reference configurations via the map $X<U^{-1} \hat{X}_{f}$ so that the class of admissible deformation gradients is $7_{a}$ for phase a and $7_{p} U$ for phase $p$. Then in terms of the deformation gradients $F_{a}<\hat{F}_{a}$ and $F^{\wedge} \hat{T} A J$ relative to the
 bearing in mind (A10), (All) becomes

$$
\begin{equation*}
\mathbf{H}(\mathbf{x}) \mathbf{P}_{\mathbf{a}}(\mathbf{x}) * \mathbf{Q P}_{\mathrm{a}}(\mathbf{x}) \quad \text { for some } \mathbf{Q c P}\left(\mathfrak{£}_{\mathrm{a}}\right)^{+} . \tag{A12}
\end{equation*}
$$

Thus the definition of coherency used in the body of the text - in which the group $9{ }^{\circ} \mathrm{f}$ symmetry transformations is a finite subgroup of the proper orthogonal group - follows naturally within the theory discussed in this appendix, with $\$$ the point group of the parent phase.
d. Proof of the existence theorem for admissibility sets 7. The EricksenPitteri theorem

We now show that there is always an open set 7 with properties (71)-(74) for any choice of reference lattice $£$. To accomplish this we use a theorem conjectured by Ericksen [18,19,20] and proved by Pitteri [21]. ${ }^{6}$ It is convenient to sometimes write ( $\mathbf{f} \mathbf{j}$ ) as shorthand for triples $\left(f_{v} i_{2 s} i_{z}\right) € V^{2}$. Let $\mathrm{TlcV}^{3}$, let $Q$ be a tensor, and let NU 3 H ; then QII is the set of all triples (Qfj) with (fj)c7l; while MJl is the set of all triples $\left(\mathbf{M}_{\mathbf{j k}} \mathbf{f}_{\mathrm{k}}\right)$ with (fj)€3ri.

We assume for the remainder of the section that a lattice $£$ with lattice vectors ( $g_{1}, \mathrm{~g}_{2} * \mathrm{~g} 3$ ) is prescribed.

Ericksen-Pitteri Theorem. There is an open set 71c $\mathrm{V}^{3}$ with the following properties:
( $\boldsymbol{\Omega}_{1}$ ) $\left(\mathrm{g}_{1}, \mathrm{~g}_{2}, \mathrm{E}_{3}\right) \in \boldsymbol{\Omega}$;
(712) QTU3II for \&U orthogonal tensors $\mathbf{Q}$;
(713) for each McW, MTU31 or MJIn31«0;

[^1](714) if M7W71, then
\[

$$
\begin{equation*}
\text { Qgj } * \mathbf{M}_{\mathrm{jk}} \mathbf{g}_{\mathrm{k}} \text { for some } \operatorname{QcP}(\mathbf{C}) . \tag{A13}
\end{equation*}
$$

\]

A dear, concise proof of this theorem is given by Ball and James 126]. We now convert this result to one appropriate to deformation gradients by defining an open neighborhood 7 of IcLin* as follows:

7 * the set of all FcLin* such that ( $\mathrm{Fg}{ }^{\wedge} \mathrm{Fgj} . \mathrm{Fgj}$ ) lies in 71. (A14)
Then 7 defined by (A14) satisfies (72), (73), (75), and (76); and hence (72)-(74). (72) and (73) follow from (711) and (712). The following result is helpful in proving (75) and (76):

> for Fc7, Gc'ytC)*, and Metro, consistent with (A2), FGc7 ++ M7U71.

The implication MTU71 -* FGc7 follows from (A2) multiplied by F and the hypothesis Fc7. Conversely, assume that FGc7. Then, since the triples (FGgj) and (Fgj) lie in 71, we may conclude from (A2) that MTIn71*0. Thus (713) yields MJW31.

To prove (76), let Fc7, let Gc'ytC)*, and choose McTII consistent with (A2). Note that (A15) with $\mathrm{F} \ll 1$ yields the conclusion Gc7 ++ M71*71, and this and (A15) for arbitrary F yield Gc7 «* FGc7.

To establish (75), let $\mathrm{Gc}^{€} \backslash(\mathrm{JI}) \mathrm{n} 7$ and choose Matr consistent with (A2). Then (A15) yields MTU71, so that (A2) and (A13) yield G€P(£)+. Thus 7 satisfies (72)-(74).

The conditions (72)-(75) are, in a certain sense, equivalent to (711)(714) with (712) and (714) restricted to rotations, but a proof is beyond the scope of this paper.


Figure 1. The lattice, the undeformed phase regions, and the deformed body. Note the possibility of dislocations along the interface $Z$.

; Figure 2. $d X_{a}$ and $d X^{\wedge}$ are compatible infinitesimal line segments at $X_{a}$ [ $\wedge^{\wedge}$. and $\mathbf{X}^{\wedge}$ that deform to $\mathbf{d x}$, and similarly for $\mathbf{d} \overline{\mathbf{X}}_{\mathrm{a}}, \mathbf{d} \overline{\mathbf{X}}^{\wedge}$ and $\mathrm{d} \overline{\mathrm{x}}$. The interface is not infinitesimally coherent at $\mathbf{x}$ and $\overline{\mathbf{x}}$ because of dislocations.


Figure 3. A two-phase loop Iff. $W_{a}$ and $W$, are the corresponding undeformed curves.


Figure 4. The portion $C$ of the interface from $a^{*}$ * to $b^{*}$ * is coherent. The underlying material isometry is equivalent to a rotation of $B$ clockwise by $90^{*}$ followed by a suitable translation.



[^0]:    ${ }^{3}$ The concept of a turf act Burger* vector is apparently due to Frank 17 J , who restricts attention to small rotations between phases. The more general situation involving finite deformations is due to Bilby (101, who essentially derives the left side of (3.23) with $Q » 1$ as an expression for the Burgers vector. See also Brooks 18], Nye 19], Bilby, Buliough. and De Grinberg (111. Christian [12,131, Boliman (14]. Christian and Crocker 115], and Pond [16,171.
    ${ }^{4}$ Bilby. Buliough, and De Grinberg (111 were apparently the first to notice this indeterminacy of the Burgers vector.

[^1]:    *Relattd ideas appear also in the work of Schwarzenberger (23] and Parry (24,25].

